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In Re Application: Tianqing He et al.

Filing Date: 11/15/03

Examiner: Jiping Lu

Serial No: 10/714,471

Art Unit: 3749

Invention: Device And Method For Rapid Drying Of Porous Materials

## **AFFIDAVIT**

NOW COMES the undersigned, who affirms and says:

- My name is Ali Regimand. I am the president of InstroTek, Inc. and a coinventor for the Device and Method for Rapid Drying of Porous Materials filed in the United States Patent Office with Serial #10/714,471.
- 2. The Vacuum Drying Apparatus and Method disclosed and claimed in serial #10/714,471 has been successfully manufactured and marketed as the "CoreDry' by InstroTek, Inc., the company which I am President. The CoreDry is priced at \$4910 per unit and since its marketing launch in 2004, my company has sold a total of 120 units. The volume for this product is expected to quadruple in the next 3 years because of the newly developed ASTM standard, described below, and Department of Transportation Specifications currently being developed in many of the states.
- 3. CoreDry does not have a price advantage over other vacuum dryer models on the market because the CoreDry, to my knowledge, is the only vacuum dryer for porous materials like asphalt currently being sold. The CoreDry has been successful in the market because it represents an advance in the art and has provided the users a fast and more accurate method of testing asphalt samples.
- Attached as Exhibit A is the newly developed American Society for Testing and Materials (ASTM) standard practice, specifically developed for the CoreDry. To my knowledge, there are no other ASTM specifications for other Vacuum Drying Apparatus, since there are no other vacuum devices or processes available for asphalt drying.

ASTM International is one of the largest voluntary standards development organizations in the world for development of technical standards for materials, products, systems, and services. Standards developed at ASTM are the work of over 30,000 ASTM members. These technical experts represent producers, users, consumers, government and academia from over 100 countries.

ASTM standards are accepted worldwide by public and private agencies. In fact, some agencies will not allow the use of an equipment, process or material without an ASTM specification.

Due to the newly developed ASTM standard, CoreDry is now a process that is internationally recognized in the asphalt testing field. This standard further validates CoreDry as a new and useful process for accurate and fast drying of porous asphalt samples.

Attached as Exhibit B are procedures established in Colorado, Pennsylvania and a test report from Colorado regarding the CoreDry. We also know that Florida and Alabama are currently developing specifications for the CoreDry, with others states following close behind. These documents and specifications further independently validate the CoreDry technology and the advance in the art represented by the CoreDry technology and patent application, serial #10/714,471.

THE AFFIANT, first being warned that willful false statement and the like are punishable by fine, imprisonment, or both under Title 28 U.S.C. 1001, states that the above information is true except those things stated on information and belief and as to those things the undersigned believes them to be true.

This the 13th day of September, 2006

An Regimand, President InstroTek, Inc.



Designation: D 7227 - 06

## Standard Practice for Rapid Drying of Compacted Asphalt Specimens Using Vacuum Drying Apparatus<sup>1</sup>

This standard is issued under the fixed designation D 7227; the number immediately following the designation indicates the year of original adoption or, in the case of revision, the year of last revision. A number in parentheses indicates the year of last respirately, epsilon (s) indicates an editorial change since the last revision or reapproval.

### 1. Scope

1.1 This practice covers the process of drying compacted asphalt specimens using vacuum drying apparatus.

1.2 The specimens dried by this practice remain at room temperature, which helps in maintaining specimen integrity during the drying process.

1.3 This practice can be used for compacted cylindrical and cubical bituminous laboratory and field specimens

1.4 This practice can also be used for drying other construction materials such as concrete, soils, aggregates and loose asphalt mixtures. Use manufacturers recommendations for drying other construction materials.

1.5 The values stated in SI units are to be regarded as the standard.

1.6 This standard does not purport to address all of the safety concerns, if any, associated with its use. It is the responsibility of the user of this standard to establish appropriate safety and health practices and determine the applicability of regulatory requirements prior to use.

### 2. Referenced Documents

2.1 ASTM Standards; 2

D 5361 Practice for Sampling Compacted Bituminous Mixtures for Laboratory Testing

## 3. Significance and Use

3.1 Specimen dry weight is a critical measure in determination of accurate density and many other tests in the construction and raw materials industries. Drying specimens at room temperature is required for some tests and provides an advantage for other tests to ensure the integrity and to preserve the characteristics of specimens.

3.2 This practice covers drying compacted asphalt specimens in a vacuum chamber that is capable of keeping the specimen at close to room temperature. A vacuum pump reduces the pressure inside the chamber, thus allowing water to evaporate at low temperature. Since the specimen naturally cools during the evaporation process, making water harder to evaporate, it is important to have proper temperature controls in the chamber to ensure specimen remains at close to room temperature. Automatic controls within the unit allow the specimen to remain at close to room temperature by periodically allowing a flow of warm air to enter the vacuum chamber. Cycling between vacuum and airflow conditions allows the specimen to dry in a short period of time. Completely saturated specimens with over 30 g of retained water can be dried in about 30 minutes. For most field cores that are not completely saturated the drying time is generally less than 15 minutes.

Note 1—Cycle time (period) can depend on the material composition. Each cycle involves an alternating period of 30 to 180 seconds of vacuum operation and 30 to 120 seconds of air flow.

- 3.3 This method can be used for 100 mm diameter, 150 mm diameter cylindrical, and cubical compacted bituminous specimens.
- 3.4 This method can also be used for drying loose asphalt mixtures, aggregate samples and other solid specimens. Follow manufacturers recommended procedures for drying specimens other than compacted bituminous specimens.
- 3.5 This method can be used to determine moisture content and amount of water loss during drying by weighing the sample before and after the drying operations.

#### 4. Apparatus

4.1 Absorptive cloth or paper towels, for drying water from surface of the specimens.

4.2 Vacuum Chamber, with a pump capable of evacuating a scaled and enclosed chamber to a pressure of 6 mm Hg, when at sea level. The chamber shall be large enough to accommodate specimens of 150 mm width or diameter and 180 mm in height. The device shall have an automatic vacuum, airflow and temperature control features to ensure proper drying of the specimen at close to room temperatures. Automatic controls of

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This precitie is under the jurisdiction of ASTM Committee D04 on Road and Paving Materials and is the direct responsibility of Subcommittee D04.21 on Specific Gravity and Density of Bimminous Mixtures.

Current edition approved Feb. 13, 2006. Published March 2006.

For referenced ASTM standards, visit the ASTM website, www.astm.org, or contact ASTM Customer Service at service@astm.org. For Annual Book of ASTM Standards volume information, refer to the standard's Document Summary page on the ASTM website.

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Fig. 1 Water Removal Plate and Sample Holder Installed in Sample Chamber

the unit shall be calibrated by the manufacturer prior to initial use. The device shall have the capability to display vacuum readings in the chamber and number of cycles.

4.3 Water Removable Plate, used for removing free water from the bottom surface of the specimen chamber.

4.4 Electronic cold trap with an airflow divider plate, used for trapping water and stopping it from entering the vacuum pump.

4.5 A handheld infrared temperature sensor accurate to ±5°C for measuring surface temperature of the specimens.

### 5. Sampling

5.1 Test specimens may be molded from laboratory prepared specimens or taken from the pavement in the field. Field specimens should be obtained in accordance with Practice D 5361.

## 6. Test Specimen

6.1 To speed up the drying process, keep and maintain the specimens to be dried between 15 °C and 30°C.

6.2 If desired, specimens may be separated from other pavement layers in accordance with D 5361.

#### 7. Procedure

7.1 Turn On the Unit:

Plug the unit in a power outlet and turn on the on/off switch. Pollow manufacturers recommendations for warm up and self test procedures.

7.2 Dally Test: Everyday before starting the testing operation, dry the cold trap and the specimen chamber. Run the unit without any specimens. The pressure reading on the display should be 6 mm Hg. or less. If the indicated pressure is higher than 6 mm. Hg. check the system for items that might need service, such as oil level and quality, seals, or water in the chamber. Refer to the manufacturer's trouble shooting instructions for obtaining a proper pressure reading in the chamber. For drying other construction materials, follow manufacturer's recommendations for pressure requirements in the chamber.

7.3 Orying Specimens: Use a handheld infrared thermometer to ensure that the surface temperature of the specimen is between 15°C and 30°C. If the specimen is below 15°C or above 30°C, place the specimens in a room temperature environment until the surface temperature approaches the required testing temperature of 15°C to 30°C.

7.3.1 Use paper towel or an absorptive cloth to remove any standing water from the surface of the specimen.

7.3.2 Place the specimen on top of the specimen support plate inside the chamber.

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7.3.3 Place the lid on the vacuum chamber and press the lid down to ensure secure contact between the lid and the chamber. Press the appropriate key, for example the Start key, to begin the drying process.

7,3.4 When the specimen is dry, the unit will automatically stop. The unit is calibrated at the factory to sense a "dry specimen condition". Dry specimen condition is determined at the factory for the pressure at which no water remains in the chamber. During testing, the unit continuously reads the pressure inside the chamber and checks this pressure against the "dry specimen condition" pressure determined during factory calibration. Follow manufacturer's procedure for calibrating the device to dry specimen condition.

Note 2—Sample is considered dry when the measured weight after vacuum drying process is 0.2 grams or less of 24-hour oven drying at

7.4 Electronic Cold Trap: Liquid and ice, or both, will accumulate in the cold trap as specimens are drying. Between drying specimens and for faster drying, it is best to remove the cold trap lid and the airflow divider plate and wipe out any free standing water in the cold trap. Always place the divider back into the cold trap before drying the next specimen.

### 8. Report

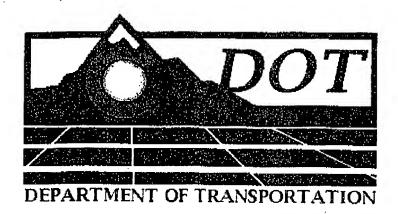
- 8.1 Report the following information:
- 8.1.1 At the end of the drying process, report the ending pressure in run Hg, to the nearest 0.1 mm Hg, and total number of cycles displayed on the screen. This information may be used by the manufacturer or the user for trouble shooting the device, if needed.

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# Review and Research of Instrotek's "CoreDry®" Report



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### PROBLEM TITLE

Using the CoreDry® to rapidly dry field cores for obtaining bulk specific gravity values:

# PROPOSED WORK PLAN

Problem Statement - Colorado DOT currently oven dries field cores for obtaining bulk specific gravity values. This method is both slow and destructive to the cores. Cores can take up to 24 hours to dry before the dry weight of the core can be taken for the Gsb (Bulk Specific Gravity) calculation. In order to properly dry cores according to CP 44 (modified AASHTO T 166), Method B, cores must be placed in an oven at 230° F and broken down, essentially destroying the core so immersed wet and surface dry weights can no longer be taken.

The CoreDry® offers two advantages over the conventional oven drying method. First, the CoreDry® only takes 15 minutes to dry a core. The current procedure calls for a minimum of 5 hours and as much as 24 hours. Gsb values are often not available the same day a core arrives in the laboratory and project personnel usually must wait overnight for test results. Secondly, the CoreDry® does not destroy the cores. This means the surface dry and submersed weights can be rerecorded if a mistake was made in this process. The cores can also be tested by multiple laboratories if there is a testing dispute.

- 1. Research Objectives The primary objective of this research is to simply evaluate if the CoreDry® compares well enough with the conventional oven dry method for use on projects.
- 2. Research Plan The following steps will be taken to accomplish the objectives of the study.
  - A. Review literature including manufacturer's data as well as other sources that have used or researched the product.
  - B. Conduct testing on cores using both methods and record the results.
  - C. Analyze data and write report.

- D. Present to MAC for approval, rejection or more investigation.
- 3. Research Plan In order to meet the objectives of this research extensive testing must be conducted on numerous cores. One constraint on the research is the amount of time we have to do the testing. The CoreDry® device we are using to conduct the research is on loan from Instrotek and needs to be returned before November 2005. Regions 3 and 5 have volunteered to conduct the testing on project cores and if time permits the central lab will also conduct testing on cores in the lab.

There is not a set amount of cores that will be tested. As many cores as possible will be tested before the CoreDry® must be returned. There are also no parameters on the cores such as aggregate grade, binder grade etc. Both 4-inch and 6-inch cores will be included in the study.

After all of the results are recorded the Gsb of both procedures will be compared for statistical analysis. Any sort of bias in either method will also be investigated.

4. Implementation — If the results in this research are found to be favorable this may be accepted as an approved product and an alternative procedure to the conventional oven drying method. An alternative procedure in CP 44 will also be drafted.

# LITERATURE REVIEW

The CoreDry® apparatus is currently only a couple years old. As a result there has not been very much research conducted on the device and there is not very much literature available for review. Other than the manufacturer's product information there has not been anything published by any transportation agency on the CoreDry®.

Joyce Stone of the Indiana DOT conducted research in the spring of 2005 on the device and was trying to publish the findings in the fall of 2005 in the Transportation Research Board Journal. Her findings are somewhat promising for the CoreDry® but her research did reveal a couple potential problems with the CoreDry®. In a draft report she stated "BSG results using the vacuum method were more consistent and generally higher than those using the standard oven drying method." According to her findings the CoreDry® is precise but not necessarily accurate. Last word is that the research has been dropped and will not be published any time soon.

The Maryland Department of Highways conducted a brief unpublished study comparing the CoreDry® to a fan dry method. It appears as though the fan dry method consists of the cores sitting in front of a fan for at least 8 hours. The CoreDry® outperformed the fan method in their study.

# TESTING PARAMETERS AND CONSIDERATIONS

For proper and accurate testing as well as evaluation of test results some basic parameters need to be considered and or assumed.

For this study field cores used on projects will be tested. The cores density will first be determined by the CoreDry® method and then by the conventional oven dry method. The CoreDry® method must always be done first since the oven dry method destroys the cores. As a result of this always being the case a bias is anticipated in the results. The CoreDry® will dry most of the water out of and off of the core initially. The oven will then dry the remaining water. This may cause a bias in the results by allowing one method to "pretreat" all the cores for the next method it is being compared to. The bias occurs because the oven dry cores have already been dried once by the CoreDry®. The cores will likely not take on much more water for the oven dry method especially if they were already bulked before the CoreDry® dried them out the first time. This pretreating could mean that the cores can only become more dry than they were before making it seem as though the oven dry cores are always less dense than they were before when taking the dry weight.

TEST RESULTS
A summary of the test results are below in Table 1.

			ComeDry	CP-44	Bulk SpG	CoreD/y	CP-44	CoreDry	CP-44	Density Density
Core #	Size	Thickness	Bulk SPG	Bulk SpG	Difference	. 53	Dry W1. (9)	(%)	Density (%)	
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 	'.	u	6 20	2.2.2		3 5011	1-85.2	67.5	53	
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4	7"	2 3:4"	2 302	7221	פיטוש	1000 6	1025.0	62	94.5	1
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Table 1 (Co	(Conti	ntinued): Summary of Results	mary of Re	sults						
Core	Size	Thickness	CoreCity Bulk SPG	CP-44 Bulk spG	Bulk SpG Difference	CoreDry Dry (VL (g)	CoreDry CP-44 Dry WL (g) Dry WL (g)	CcreDry Density (%)	CP-44 Density (%)	Density Difference (%)
70	وز	2 1/4"	2.285	2254	0.661	2262.3	2261.7	54.2	48.4	٥
ın	وز	2 1/4	2.164	2.38	0.00	2523.3	20.18	2.68	89.2	32
9	9	, trl 2	2.244	2241	0.003	2237.2	2234.	92.7	92.E	3.1
2	وز	. P/1 3	1227	2224	වා.ග	2130.7	2127.8	32	ي. زد	3.1
8	و	2 1/4	2.26	2.25	0.002	2267.5	2265.2	93.5	53.5	2.1
14351-1	ř		2.374	2.373	0.061	1436년	1435.	36.1	36.1	G
14551-2	24		2.350	2.345	0.051	1436.1	1435.2	95.2	95 1	
14551-3	শ		2.386	2352	0.064	1212.3	1210.2	96.5	88.4	32
ı	17		2,386	2.354	0.002	1041.5	1040.8	96.3	£	1
14351-5	-7		2.390	2.358	0.002	1591.1	1390.3	86.3	36.7	
14351-6	•4		2.398	2357	9.661	1161.1	6.031	97.1	97 C	3.1
14331.7	-		2.382	2.351	1.30.0	1820.3	: 520.3	5.05	95.4	C
14551.8	وز		2.285	2.28	0.005	2215.3	2211.5	92.5	92.3	32
14351-9	و		2.248	2.247	0.081	2215.3	:6825	6.3	90 E	25
14851-10	وز		2.23	2.215	0.038	22155	· 546.4	89.7	85.7	5 ,
14851-1	و		2.224	2.221	0.003	2215.3	22825	85.3	£ 68	
14851-12	ی		2.220	2.218	0.002	2215.3	2.154.4	89.5	388. 2	-
14851-13	فا		2.244	2.24	0.004	2215.3	2133.2	500.5	50.4	7.5
14851-14	و		2.170	2.755	0.061	2215.3	2164.9	87.5	87 £	0
14851-15	ت		2.258	2256	0.002	2215.3	2580.	9.2	i. Š	c
14851-16	9		2.256	2.254	D.C62	2215.3	2269.8	91.1	37.66	
14851-17	ట		2.206	2.2.4	0.002	2215.3	2558.5	89.1	368	
14851-18	9		220	2.35	D.C02	2215.5	3673.	88.3	88.č	
14851-19	9		2.198	2.36	0.02	2215.5	20802	88.7	88.7	2
14851-20	S		2256	2.253	0.003	2215.3	32028	9.1	9. C	5
14851-21	ؽ		2.190	2.57	D.C03	2215.3	2Ē19.8	88.4	\$8 %	
14314-1	-4		2.250	2.255	-C.00:3-	85e	556.5	54.5	귏	-0.2 -0.2
143142	ন		2.3.	2.354	0.007	748.6	747.5	97.2	396	200
14314.3	*4		2.237	2.233	0.004	788.8	787.2	3	326	7 .
14314-4	- <del>-</del> -17		2.279	2.275	9.C04	6.035	5:59.8	95.3	85	~

Table 1 (Continued): Summary of Results

CP-44  See 19 19 19 19 19 19 19 19 19 19 19 19 19											
4         2256         2254         3.002         365         3636         94         3625         97.6	Ccre#	Size	Thickness	Coredry Bulk SPG	CP 44 Bulk SpG	Bulk Sp.G. Differe ace	CoreDry Dry VA. (g)	CP:44 Dry Wt (g)	Corellry Density [%]	CP-44 Dens fty (%)	Derisky Oifference Pki
4         2.25         2.24         3.04         8.24         9.6         9.				2006. 2	1 2 E	600 8	25.5	3638	7.5	38.8	0.1
4         17.8°         2.250         2.277         0.0°3         32.48         8/2.2         9/2.2         3.9°	14:476-0	4		CC77	4777	200.5	3				ربر ح
4         178         2250         2254         0.006         30.36         30.27         36         349           4         178         2222         222         3.07         763.8         70.6         93.4         52.2           4         2         2.226         2.275         3.0°         743.8         767.9         94.8         54.2           7         4         2         2.226         2.273         3.0°         743.8         747.9         94.8         54.2           7         4         2         2.221         2.213         0.0°         762.9         701.5         94.8         54.2           7         4         1.78         2.220         2.243         0.0°         762.9         701.5         94.8         54.2           7         4         1.78         2.220         2.243         0.0°         762.9         701.5         94.5         55.2           8         1.78         2.220         2.221         3.0°         76.7         775.1         95.9         96.3           6         1.78         2.220         2.220         3.003         184.6         184.4         91.9         34.7           6 <th>144126</th> <td>-4</td> <td></td> <td>2.320</td> <td>2322</td> <td>0.0.3</td> <td>324.8</td> <td>822.2</td> <td>97.5</td> <td>5,</td> <td>2 0</td>	144126	-4		2.320	2322	0.0.3	324.8	822.2	97.5	5,	2 0
4         178         223         222         90.2         763.8         70.6         95.4         92.3         52.3           4         7         2.256         2.275         90.2         779.7         778.2         95.7         55.2           7         4         2         2.226         2.275         90.3         749.8         747.9         94.8         64.2           7         4         2         2.226         2.243         90.9         76.6         92.4         92.2         52.2           8         4         1.78         2.259         2.243         90.1         76.7         76.3         96.2         92.8           9         4         1.78         2.259         2.243         90.1         76.7         76.5         96.2         96.3           4         1.78         2.259         2.243         90.1         76.7         76.7         76.5         94.5         94.7           5         1.78         2.256         2.266         3.003         186.7         184.4         91.9         34.7           6         1.78         2.264         2.263         2.006         178.6         146.4         94.5         35.	14976-7	-1		3.250	2.254	0.005	3.63.6	: 708	9 <u>2</u>	3.75	۱۹۲
4         178*         2252         222         90*2         763.8         70.6         93.4         523.           4         2         2256         2275         90*3         779.7         778.2         93.7         55.3           7         4         2         2266         2273         90*3         783.6         747.9         94.8         54.2           7         4         2         2264         2273         90*3         767.9         94.8         54.2           7         4         2         2264         2243         90*6         767.9         70*6         94.8         54.2           7         4         178*         2259         2243         90*1         767.3         70*6         94.5         55.2           7         4         2         2254         2273         90*1         776.7         94.5         94.3         54.7           6         178*         2256         30*1         178*5         178*1         94.3         34.7           6         134*         226         30*1         178*2         95.3         34.7           6         178*         23*6         226         30*1											
4         150         2.252         2.275         3.0 2         779.7         778.2         95.7         25.2           4         2         2.296         2.275         3.0 3         743.8         747.9         94.8         34.2           7         4         2         2.227         2.213         0.003         783.6         79.4         94.8         54.2           7         4         2         2.227         2.213         0.016         70.29         70.5         94.8         54.2           7         4         1.78*         2.259         2.243         0.066         70.29         70.5         94.5         55.2           6         4         1.78*         2.259         2.279         0.01         76.7         775.1         95.9         56.7           6         1.78*         2.226         2.279         0.003         18.97         18.42         91.9         31.8           6         2.38*         2.266         2.061         175.6         175.3         93.5         35.2           6         1.38*         2.376         2.061         175.6         175.9         93.5         35.2           6         1.78*	300		100.2	2 325	2, 6	6.70 6	8 535	9 111	93.5	523	30
7         2.25         2.25         0.0 2         7.31         10.2         2.27         2.26         2.27         2	14814-1	3	Q'1	2525	777	3.0.5	200	2 8/1	C ± 2	177 187 17	30
7         2         2.256         2.263         3.0°3         745.8         4.0°4         940         54.8           7         4         2         2.277         2.213         0.009         763.6         767.3         767.3         940         54.2           7         4         17.8°         2.259         2.243         0.0°6         762.9         70°5         945         55.2           7         4         17.8°         2.259         2.263         0.0°1         767.3         76.3         96.2         56.3           6         17.8°         2.29         2.273         0.0°2         77.6°1         95.9         56.4           6         17.8°         2.22         0.0°3         188.7         1644.4         91.9         34.7           6         2.8°         2.26         0.0°3         188.7         1644.4         91.9         34.2           6         1.8°         2.2°         0.0°3         186.7         1644.4         91.9         34.2           6         1.8°         2.2°         0.0°         1750.5         1750.5         94.5         35.2           6         1.78°         2.3°         2.2°         0.0° <th><b>乙字16</b>秒</th> <td><del></del></td> <td>2</td> <td>2.75</td> <td>6.275</td> <td>5.U.2</td> <td>175</td> <td>701</td> <td>- 3</td> <td></td> <td>) U</td>	<b>乙字16</b> 秒	<del></del>	2	2.75	6.275	5.U.2	175	701	- 3		) U
7         4         2         2.227         2.213         0.009         783.6         782.4         91.2         92.2           8         4         17.8         2.259         2.243         0.0°6         702.9         701.5         94.5         55.2           7         4         17.8         2.259         2.243         0.0°6         767.3         766.5         96.2         56.3           8         4         2         2.259         2.273         0.0°6         767.3         775.1         97.9         56.4           6         7.78         2.256         2.276         6.003         1887         1646.4         91.9         34.7           6         2         2.26         2.266         6.003         1887         164.4         91.9         34.5           6         2         2.26         2.001         1786.5         1734.3         91.5         35.2           6         1.32         2.26         6.002         1786.9         1756.3         95.5         35.2           6         1.78         2.36         2.265         6.001         1750.9         1756.3         95.5         35.2           6         1.78	18 to	-7	74	3.236	2.253	5.0.3	745.8	57.57.	33	24.5	, ,
3         4         17.8°         2259         2243         6.0°6         7629         7015         945         55.2           4         17.8°         2259         2259         6.0°1         7673         7665         945         55.2           5         4         2         2259         2269         6.0°1         7673         7665         95.2         56.3           6         1.78°         2.256         2.269         6.003         1889         16862         94.5         34.7           6         2         2.26         2.266         2.266         6.003         1887         1644         91.9         31.8           6         2         2.26         2.061         1786.5         1734.3         92.5         36.7           6         1.32°         2.26         6.001         1786.9         1756.3         93.5         36.2           6         1.78°         2.37°         2.26°         6.001         1786.9         1726.9         94.5         36.2           6         1.78°         2.37°         2.26°         6.001         1760.9         1726.9         93.5         35.2           6         2°         2.264	1.4 Cal . 1.4	7	2.	7777	2.213	0.003	75.3.6	4.20.4	92.2	375	200
5         4         17.8°         2.259         2.259         0.0°1         7673         7665         96.2         56.7           5         4         7         2.259         2.259         0.0°2         776.7         775.1         95.9         56.4           6         1.78°         2.258         2.226         0.003         1889         1680         96.2         34.7           6         2.18°         2.256         2.226         0.003         18.7         1644         91.9         31.8           6         2.18°         2.266         2.267         0.001         1785.6         1734.3         91.9         31.8           6         1.32°         2.264         2.262         0.002         168.9         169.5         31.2         35.2           6         1.38°         2.265         0.001         1786.9         1726.3         94.5         35.2           6         1.78°         2.376         2.265         0.001         1750.9         1726.3         95.3         35.2           6         2.264         2.264         2.261         0.003         166.8         1726.3         93.4         35.2           6         2.	240.4.62	-	48.7	7.954	2.043	3.0.6	702.9	70:5	94.5	13 13 13 13 13 13 13 13 13 13 13 13 13 1	ارد
6         2         2254         2273         6.0°2         776.7         776.7         775.1         95.9         86.4           6         2         2256         2275         6.003         188.9         184.4         91.9         31.2           6         2         2256         2275         6.003         18.7         184.4         91.9         31.2           6         2         2266         2275         6.001         178.5         134.3         91.9         31.2           6         134.*         2264         2225         6.002         180.5         160.5         150.5         94.5         35.2           6         138*         2376         230.9         6.001         1786.4         1494.4         94.5         35.2           6         178*         2376         230.9         1786.4         1780.9         1720.9         94.5         35.2           6         178*         237         226.1         0.001         1780.9         1720.9         93.2         35.2           6         2         2264         2264         2261         0.001         1780.9         1720.9         93.2         35.2           6	2 + 1373	-	81.5	3.934	EBC C	9.00	757.3	756.3	95.2	56.5	n
6         17.8°         2.256         2.226         2.226         2.226         3.226         3.226         3.226         3.226         3.226         3.226         3.226         3.226         3.226         3.226         3.226         3.226         3.226         3.227         3.061         1784.4         91.9         31.5           6         2         1.8°         2.266         2.061         1785.5         1743.3         93.4         35.2           6         1.58         2.286         2.265         0.001         1750.9         1720.3         95.3         34.2           6         1.78°         2.37°         2.31°         0.001         1750.9         1720.3         95.3         35.2           6         2         2.264         2.281         0.003         1846.8         1941.5         93.4         35.2           6         2         2.264         2.281         0.003         1846.8         1941.5         93.4         35.2	140 H	-	200	7.254	2.079	9.0.2	7.6.7	175.1	97.9	म 93	÷0
6         1.7.8°         2.29         2.269         6.003         1669.6         1662         94.5         34.7           6         2.38         2.226         2.226         6.003         16.7         1644.4         91.9         31.8           6         2         2.266         2.267         6.001         1785.5         1741.3         91.9         31.8           6         13.2°         2.264         2.262         6.001         160.9         160.9         160.5         36.2         36.2           6         13.8°         2.3°         2.2°         6.001         1750.9         1720.9         94.5         36.2           6         17.8°         2.3°         6.001         1750.9         1720.9         94.5         36.2           6         17.8°         2.3°         2.2°         0.001         1750.9         1720.9         93.2         35.2           6         2°         2.2°         2.2°         0.003         1946.8         1946.8         93.4         35.2           7         2.2°         2.2°         0.004         10.004         10.004         10.004         10.004         10.004         10.004         10.004         10.004	1.41.1.24.1	,	7								
6         1 7.8°         2.256         2.226         3.003         155.5         505.4         91.9         31.5           6         2 .8°         2.256         2.256         3.061         1785.5         1734.3         92.5         35.5           6         2 .8°         2.264         2.267         0.061         1785.5         1734.3         92.5         35.5           6         1 32°         2.264         2.265         0.061         1466.4         1494.4         94.5         34.2           6         1 78°         2.376         2.265         0.001         1760.9         1726.9         93.5         35.2           6         2°         2.264         2.261         0.003         1546.8         1946.5         93.4         35.2           6         2°         2.264         2.261         0.003         1546.8         1946.5         93.4         35.2							2000	6 35 23	63.5	77.	30
6         2         3229         2226         3.063         1847         16444         91.3         5.1           6         2         2.256         2.257         0.061         1785.6         1734.3         91.3         5.1           6         132*         2.264         2.252         0.061         1785.6         1707.5         92.4         35.2           6         1 58*         2.286         2.255         0.001         1756.4         1494.4         94.5         34.2           6         1 78*         2.376         2.355         0.001         1750.9         1720.9         93.4         35.2           6         2**         2.264         2.261         0.003         1646.8         1641.5         93.4         35.2           6         2**         2.264         2.261         0.003         1646.8         1641.5         93.4         35.2	1257	.e	.8.2	2.238	× 151.3	5.003	1203.5	70201	5 2	0 1/2	0.1
6         2         2.256         2.257         0.061         1785.6         1734.3         93.0         50.0           6         132*         2.264         2.252         6.002         1508.9         1507.5         93.4         55.2           6         1.58*         2.296         2.255         0.001         1750.9         1726.9         94.5         34.2           6         1.78*         2.37         2.255         0.001         1750.9         1726.9         95.5         35.2           6         2*         2.264         2.261         0.003         1646.8         1641.5         93.4         35.2           Average         0.004         0.004         0.004         0.004         0.004         0.004         0.004	32.57	6	.80	2.236	2.225	3.063	[8.7]	1544.4	7: 55 50	1 1 1	;   ;
6         132*         2264         2222         6.002         1508.9         1507.5         93.4         53.7           6         138*         228*         228*         6.001         1496.4         1494.4         94.5         34.2           6         178*         237*         230*         6.001         1750.9         1728.9         95.3         35.2           6         2*         2264         2261         0.003         1846.8         1844.5         93.4         55.2           Average         0.064         0.064         1.003         1.064         1.003         1.004	1:67	ء	2.	2.236	2.283	30.6	1735.5	[1343	92.5	1) (c) (c) (c) (c) (c) (c) (c) (c) (c) (c	2 2
6         158*         228*         226*         9.001         14654         1494*         94.5         54.2           6         178*         23°         23°         0.001         1760.9         1726.9         95.3         36.2           6         2*         2.264         2.261         0.003         1646.8         1944.5         93.4         35.2           Average         0.004         0.004         0.004         0.004         0.004         0.004	4.57.4	عاد	132.	2.284	2.252	0.082	1568.9	1507.3	93.2	3.65.5	2 2
6         17.8°         2.3°         2.0°         1750.9         1720.9         55.2           6         2°         2.264         2.261         0.003         1646.8         1844.5         93.4         35.2           Average         0.064	1:67	בי	15.8	3.235	2.265	0.001	1456.4	ा हैन	94.5	5. 4. 5.	* C
6 2* 2.264 2.281 0.003 1846.8 1844.8 93.4 35.2	1:67	יב	.8.1	13.87	2.223	1.00%	1730.5	17293	97.3	200 200 200 200 200 200 200 200 200 200	100
Ave 326 0.064	1.67	9 (4)		2.264	1327	0.003	1546.8	1944.5	93.2	335	٥٢
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\*Cores on project 14914 were bulked by two different testers for the CoreDry® and the Oven Dry method

# ADDITIONAL TESTING AND RESULTS

After the initial testing was concluded and the results recorded in Table 1, additional testing was needed to examine if the bias is an outcome of the circumstances or if the oven dry method is actually more effective than the CoreDry® method.

The additional research was conducted to try and take out the bias or the advantage the oven dry method has by always going after the CoreDry® method. Twelve samples were put under a vacuum for 90 seconds and saturated with water much like the Moisture Susceptibility test in Colorado Procedure 5109. The weight of the sample was taken before saturation, after saturation and then again after the sample was dried. This determined how effective each method is in removing water from the samples. The two methods were then compared in how efficient they are in removing water as a percentage.

While conducting the extra testing the CoreDry® did not appear to completely dry some of the samples. The weight was noted and the sample was dried again. This may not be anything major since the CoreDry® is not designed to dry vacuum saturated design samples and the apparatus may have been overloaded but it may have to be written into the procedure to check the core for any residual water on the surface and dry the core again if moisture is visible.

Table 2: Results for Extra Testing with the CoreDry®

				CoreDry		
Sample Number	Original Weight (g)	Saturated Weight (g)	Water Added (g)	Dried Weight (g)	Water Removed (g)	Efficency (%)
391-1	1168.6	1183.2	14.6	1169.5	13.7	93.8%
391-2	1168.4	1181.9	13.5	1169.1	12.8	94.8%
391-3	1169.5	1184.1	14.6	1170.5	13.6	93.2%
399-1	1165.6	1176.9	11.3	1107.3	9.6	85.0%
399-2	1165	1176.1	11.1	1166.8	9.3	83.8%
399-3	1165.8	1176.6	10.8	1167.7	8.9	82.4%
400-1	1144.9	1155.6	10.7	1146.7	8.9	83.2%
400-2	1145	1155.9	10.9	1146.7	9.2	84.4%
400-3	1144.8	1154.9	10.1	1146.6	8.3	82.2%
408-1	1155.1	1161.1	6	1155.9	5.2	86.7%
406-2	1154.6	1160.3	5.7	1155.4	4.9	86.0%
406-3	1154.2	1163.4	9.2.	1155.3	8.1	88.0%

Average 86.9%

Table 3: Results for Extra Testing with the Oven

				Oven Dry				
Sample Number	Original Welght (g)	Pan Tare (g)	Saturated Weight (g)	Water Added (g)	Pan+ Sample (g)	Dried Welght (g)	Water . Removed (g)	Efficency (%)
004.4	4469.6	249.3	1183.4	14.8	1419.1	1169.8	13.6	91.9%
391-1	1168.6 1168.4	248.4	1182.2	13.8	1418	1169.6	12.6	91.3%
391-2		254.9	1184.6	15.1	1425.7	1170.8	13.8	91.4%
391-3	1169.5	251.9	1177.7	12.1	1418.4	1166.5	11.2	92.6%
399-1	1165.6	254.7	1176.5	11.5	1420.4	1165.7	10.8	93.9%
399-2	1165_ 1165.8	244.6	1177.4	11.6	1411.4	1166.8	10.6	91.4%
399-3	1144.9	248.7	1157.8	12.9	1394.7	1146	11.8	91.5%
400-1 400-2	1145	252.1	1157.7	12.7	1398.2	1146.1	. 11.6	91.3%
400-3	1144.8	255.1	1155.5	10.7	1401	1145.9	9.6	89.7%
406-1	1155.1	251.4	1161.4	6.3	1407.1	1155.7	5.7	90.5%
406-2	1154.6	256.9	1160.7	6.1	1412.2	1155.3	5.4	88.5%
408-3	1154.2	254.4	1164.2	10	1409.6	1155.2	9	90.0%

Average 91.2%

## RESULTS SUMMARY

When comparing field cores the average difference in density comes out to be 0.17% and never exceeded a difference of 0.6%. The average Bulk Specific Gravity difference is .004 and never exceeded .016. When conducting the extra testing on design samples the CoreDry® removed 86.9% of the water added while the oven removed 91.2%.

The densities between the two methods were plotted below and an "R" squared value was determined to be .9969.

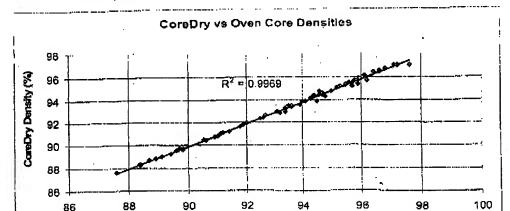


Chart 1: CoreDry® Versus Oven Dry Densities

A  $T_{paired}$  Test was conducted on the densities and showed no statistical difference between the two methods.

Oven Dry Density (%)

t paired = d bar / (Sd /sq rt n)

d bar = 3.76 / 76 = .0495

Sd squared =  $3.76 - (13^2/76) = 1.536$ 

Sd = 1.239

Sq rt n = sq rt 76 = 8.718

t paired = .0495/(1.239/8.718)=.3483

T.05, 76 = 1.668

Since .3483 is less than 1.668, the data strongly suggests there is no difference in densities.

## CONCLUSION

Based on the data analysis it is recommended that the CoreDry® apparatus be accepted as an alternative to the oven dry method (Method B) of CP 44.

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Commonwealth of Pennsylvania Department of Transportation

PA Test Method No. 715LA Revised Feb. 2006 5 Pages

#### Method of Test for

# DETERMINATION OF BULK SPECIFIC GRAVITY OF COMPACTED BITUMINOUS ROADWAY CORE SAMPLES

### 1. SCOPE

1.1 This method of test is intended for determining the bulk specific gravity of bituminous roadway core samples obtained for and governed under the Local Acceptance specification only.

### 2. TEST SPECIMEN

- 2.1 Core samples from the compacted pavement obtained in accordance with PaDOT methods of sampling a compacted roadway.
- 2.2 Specimen size It is recommended, (1) that the diameter of the cored specimen be at least equal to four times the nominal maximum size of the aggregate; and (2) that the thickness of the core be the actual depth of the material as placed on the project or at least 1.5 times the nominal maximum aggregate size.
- 2.3 Specimens shall be free of foreign materials such as seal coat, tack coat foundation material, soil and any other material not a component of the original mix.

## 2.4 Sample Preparation

- 2.4.1 Specimens are to be separated from other pavement layers by sawing or other suitable means. Care shall be exercised to ensure separation does not damage the specimen.
- 2,4.2 Specimens shall be dried to a constant mass (constant mass shall be defined as the mass that is obtained when further drying does not alter the observed mass by more than 0.05 percent) using one of the procedures described:

- (1) Dry the sample for at least 20 hours at  $52 \pm 3^{\circ}$ C ( $125 \pm 5^{\circ}$ F), checking the dry weight at two hour intervals until constant mass is reached.
- (2) Dry the sample in a large, flat pan of known mass in an oven at  $110 \pm 5^{\circ}$ C (230  $\pm$  9°F) until the fine aggregate-asphalt portion can be separated into pieces no larger than 6.4 mm (1/4 in.). Return the sample to the oven, checking the dry weight after cooling to room temperature [25  $\pm$  5°C (77  $\pm$  9°F)], every half hour until constant mass is attained on at least three consecutive weighings. Note: Caution should be exercised before using this method since the sample will be destroyed by this process. Samples coated with paraffin cannot be prepared by this method.
- (3) Dry the sample by exposure to moving air of relatively low humidity while changing the orientation of the sample frequently and checking the dry weight every half hour until constant mass is attained on at least three consecutive weighings.
- (4) Dry the sample in a vacuum drying apparatus meeting the requirements of, and in accordance with, ASTW D-7227-06.

## 2.5 Verification

2.5.1 Use methods 2.4.2(3) and 2.4.2(4) as preparation for acceptance testing only after verification in accordance with the appropriate specification.

#### VOLUMETER METHOD

### 3. APPARATUS

- 3.1 Weighing Device Conforming to the requirements of AASHTO M-231, Class G2.
- 3.2 Thermostatically controlled water bath designed to maintain the bath temperature at  $25 \pm 0.5$ °C (77  $\pm 0.9$ °F)
- 3.3 Thermometer ASTM 17C (17F), having a range of 19 to 27°C (66 to 80°F), graduated in 0.1°C (0.2°F) subdivivsions
- 3.4 Volumeter Calibrated, 1.2L or an appropriate capacity depending on the sze of the sample.